

**2nd International Conference on Structured Catalysts and Reactors  
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Delft, The Netherlands**

# **Optimization of anodic oxidation and Cu-Cr oxide catalyst preparation on structured aluminum plates processed by electro discharge machining**

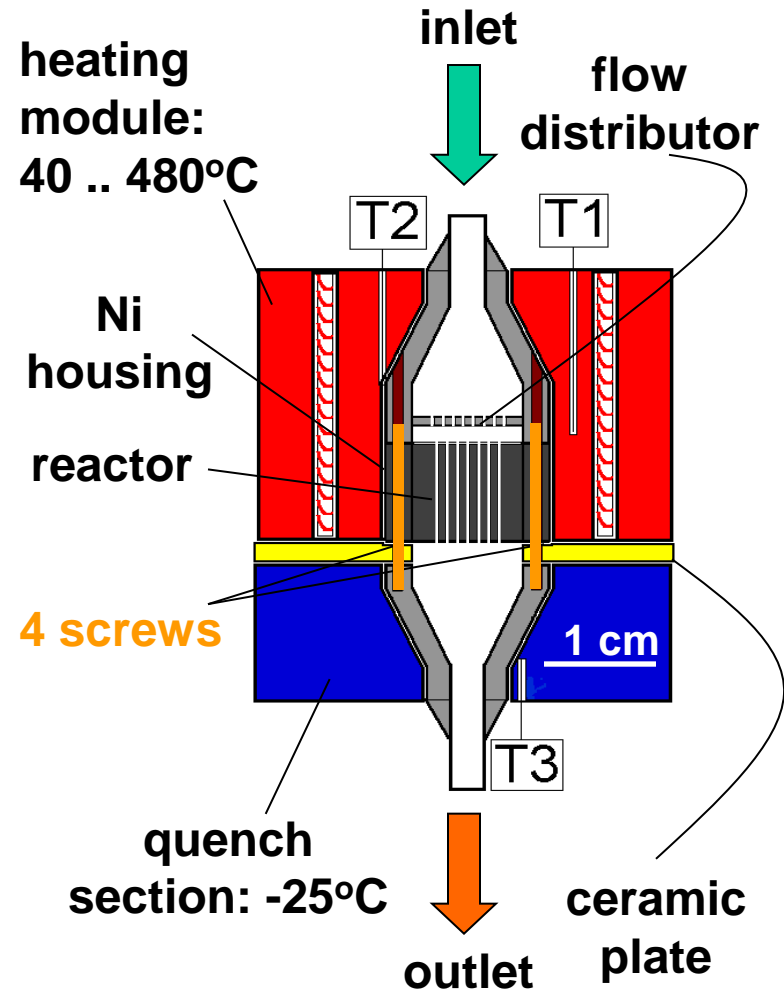
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# Introduction

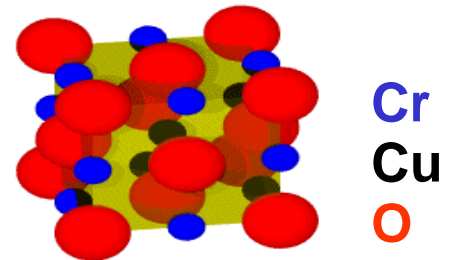


(E.V. Rebrov et al.,  
Catal. Today 69 (2001) 183)

Microreactors: tools for both basic research and safe process development, opportunity to safely study the kinetics of catalytic total oxidation:

- small unit size
- channel diameter < 500  $\mu\text{m}$  (large surface-to-volume ratio) => gas-phase reactions, including explosive ones, can be avoided
- highly exothermic reaction => efficient heat removal

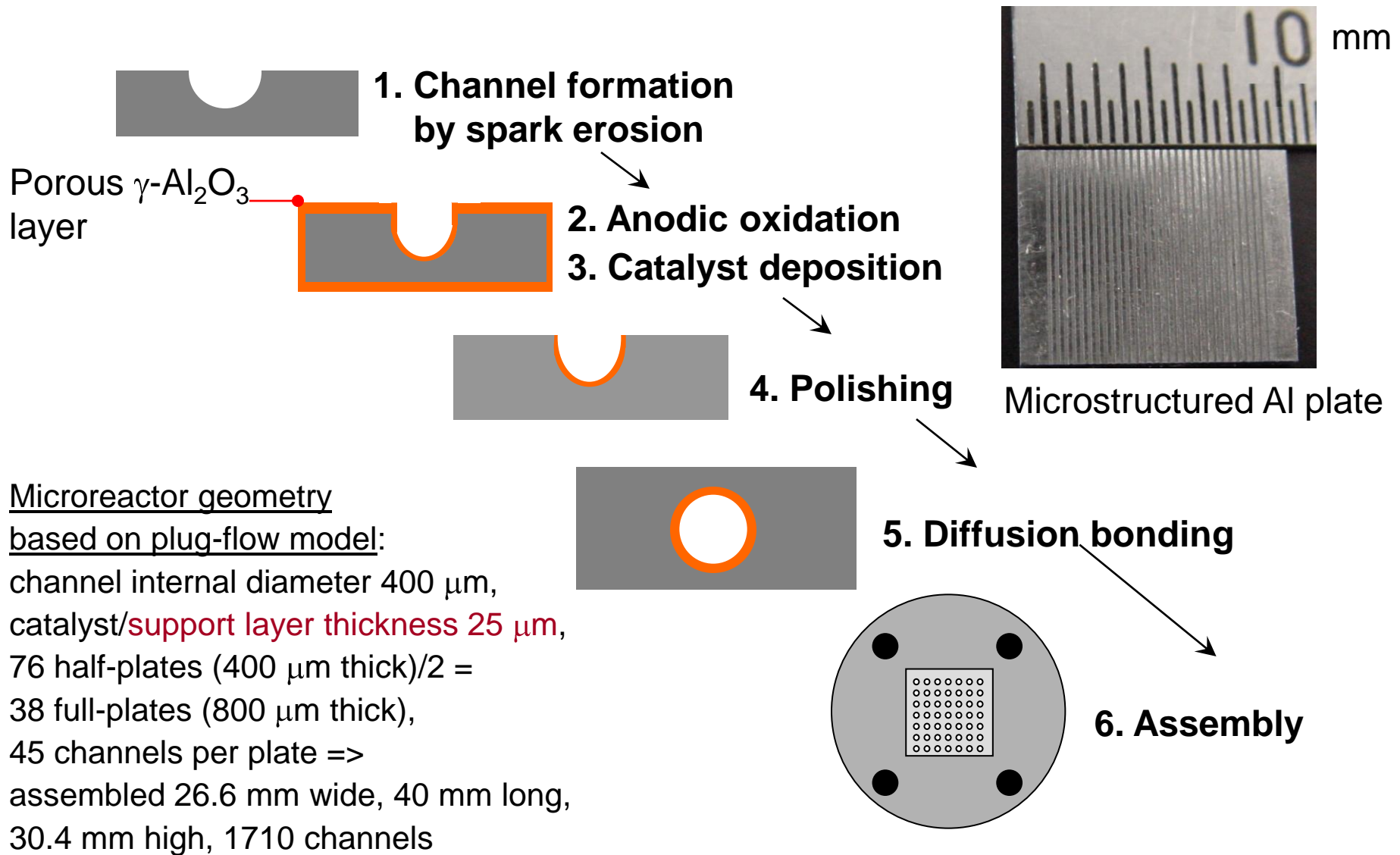
- Spinel catalyst  
 $\text{CuCr}_2\text{O}_4/\gamma\text{-Al}_2\text{O}_3$   
high oxidation activity



# Outline

- Fabrication and characterization of microstructured plates
  
- Anodic oxidation of metal plates
  - Oxidation of flat aluminum plates
  - Adaptation of oxidation procedure with the AlMgSi1 alloy
  
- Development of preparation methods of catalytic coatings
  - Preparation of Cu-Cr oxide catalytic coatings on flat aluminum plates
  - Adaptation of catalysts synthesis procedure for microstructured plate

# Microreactor fabrication



# Fabrication of microstructured plates

## **Al microreactor material:**

**high heat conductivity (230 W/m·K)**

- **can be used up to 450 °C (m.p. 660 °C)**
- **microchannels easily made (e.g., by spark erosion)**
- **anodic oxidation allows formation of external porous g-Al<sub>2</sub>O<sub>3</sub> layer for catalyst active component deposition**

## ■ **Material**

- **Al 99.5**

- **AlMgSi1 alloy**

**(Al51 st)**

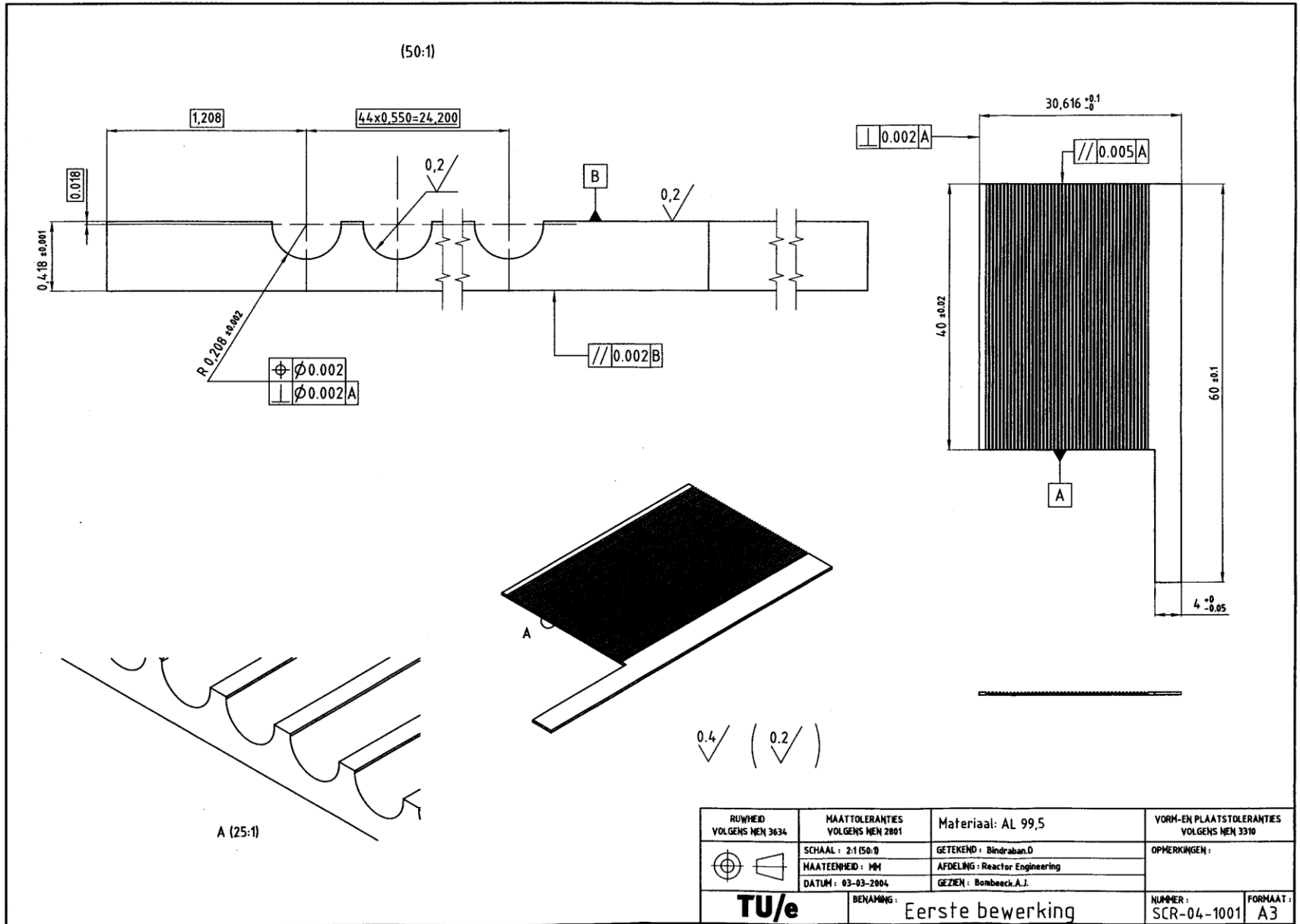
## ■ **EDM procedure**

- **1 incision**

- **2 incisions**

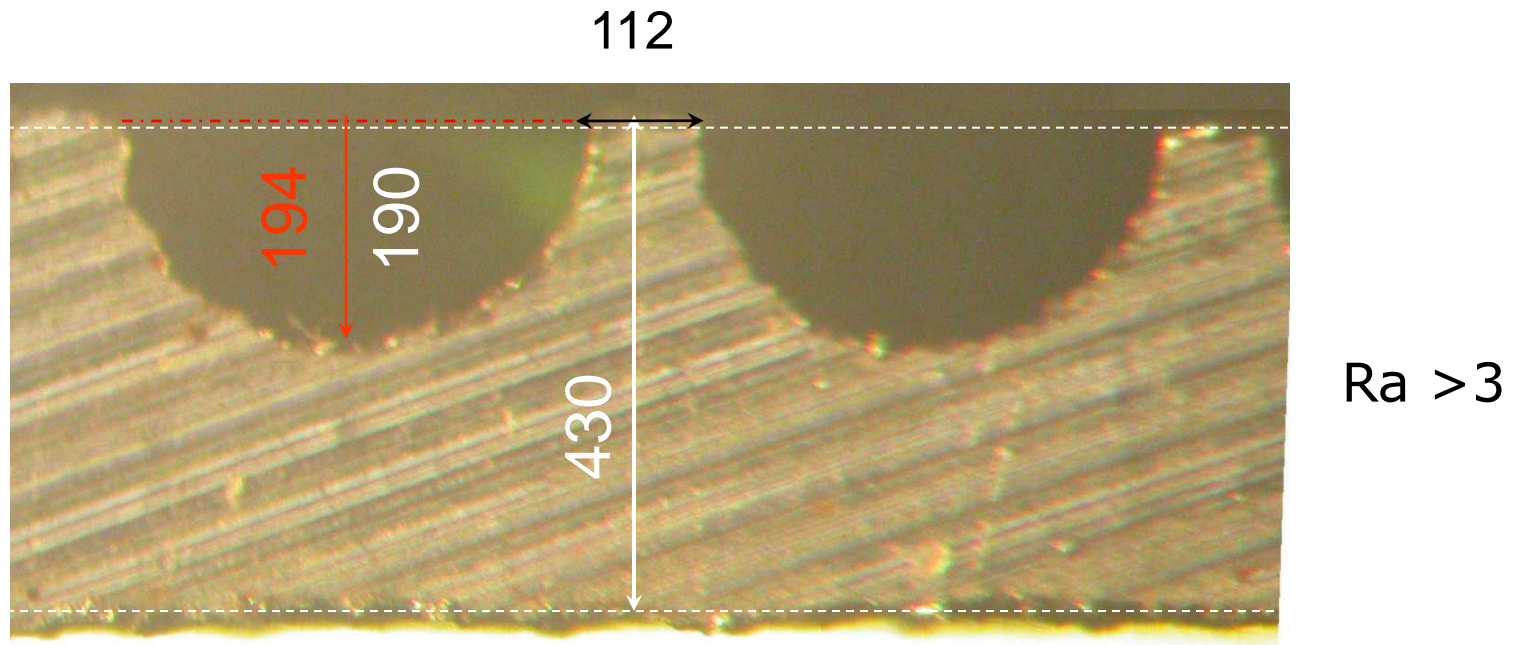
- **3 incisions**

# Single sided plates h = 0.42



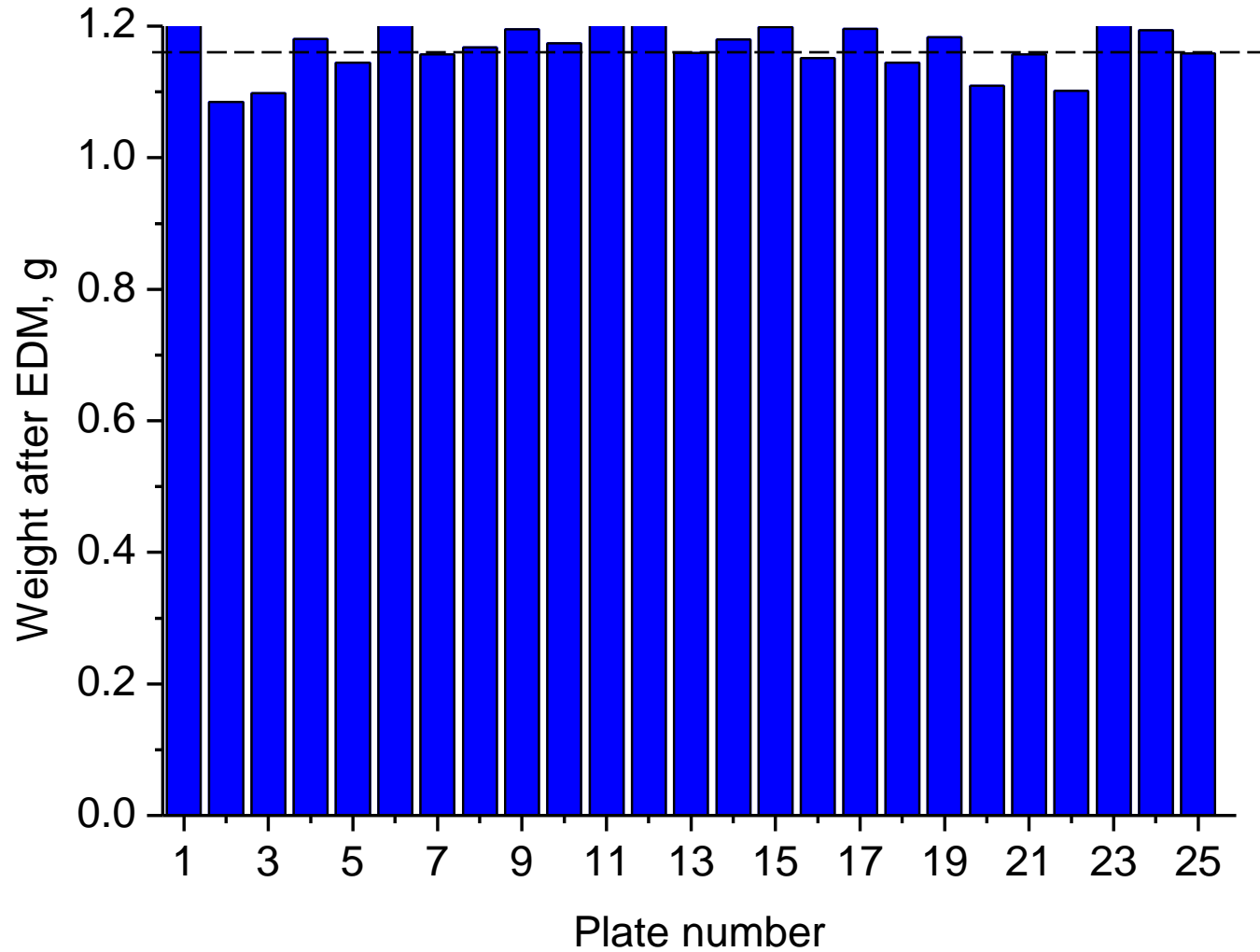
# Fabrication of microstructured plates

- 1<sup>st</sup> series: 21+63 microstructured plates (1 incision)



Dimensions: 45 channels with  $R=208$  micron,  $L = 40$  mm

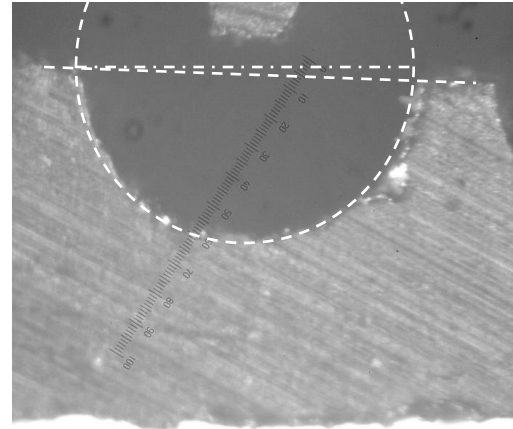
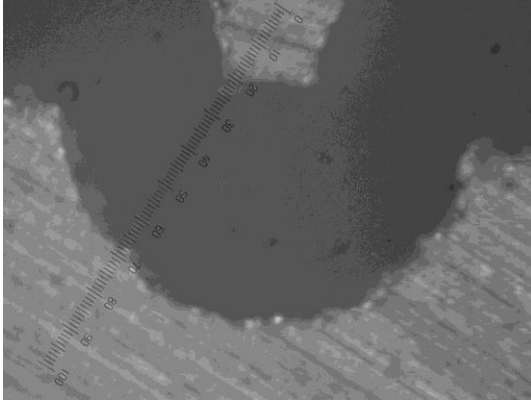
# Plate weight after EDM





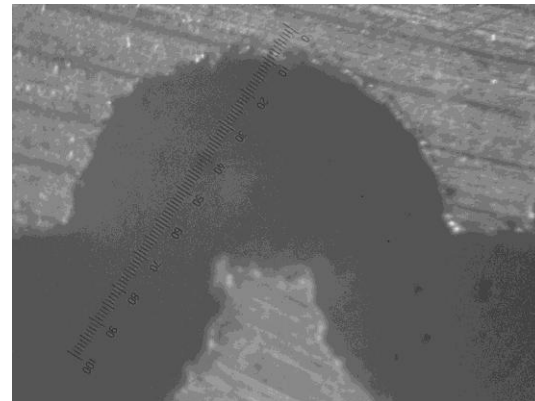
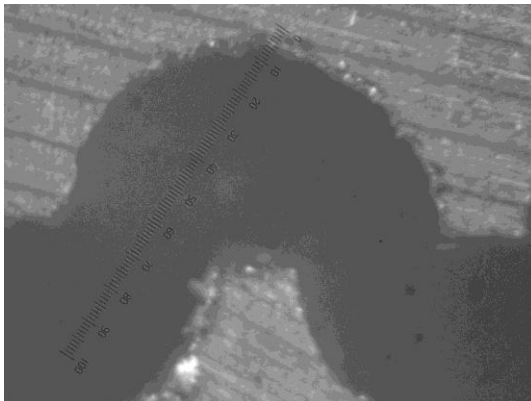
## 2<sup>nd</sup> series

2 incisions



Ra = 2.0

2 incisions + micro-powder jet treatment

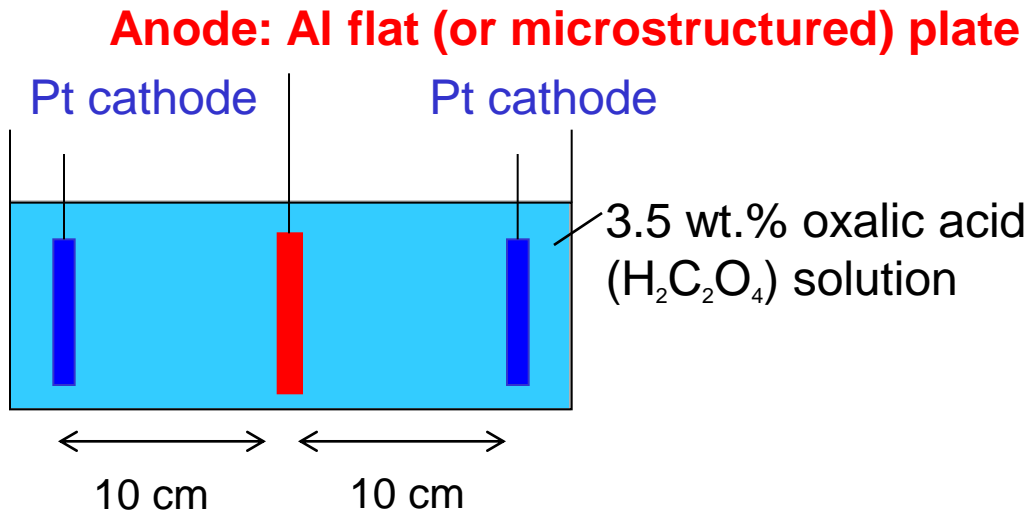


Ra = 2.0

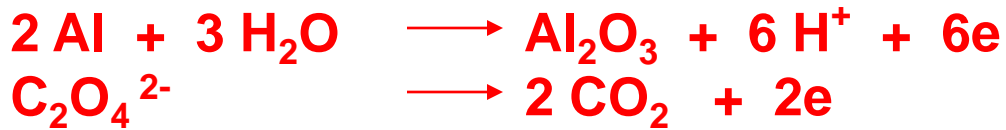
## Summary

- Fabrication of long (40 mm) microchannels in Al 99.5 (code:1050A) is not possible
- Method "1 incision" gives surface roughness  $R_a > 3.2$  with the Al51st alloy
- It is possible to reach  $R_a = 2.0$  with fabrication method "2 incisions" in Al51st

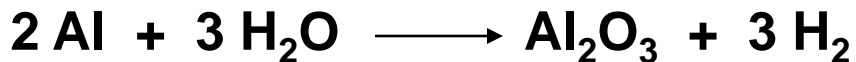
# Anodic oxidation



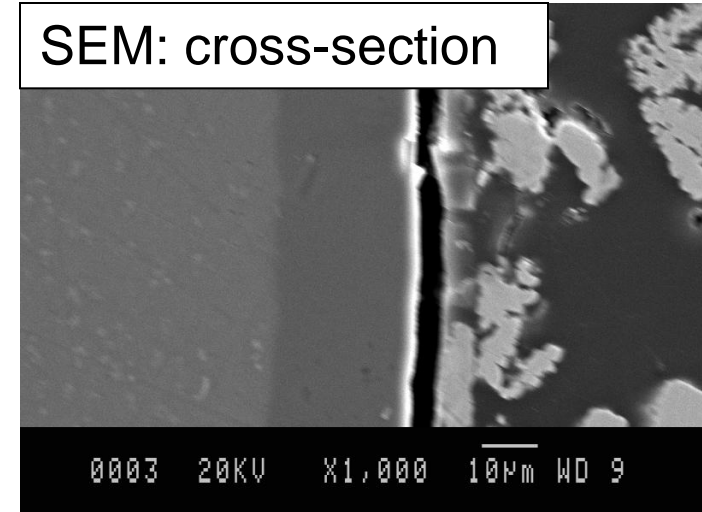
**Anode:**



**Cathode:**



SEM: cross-section

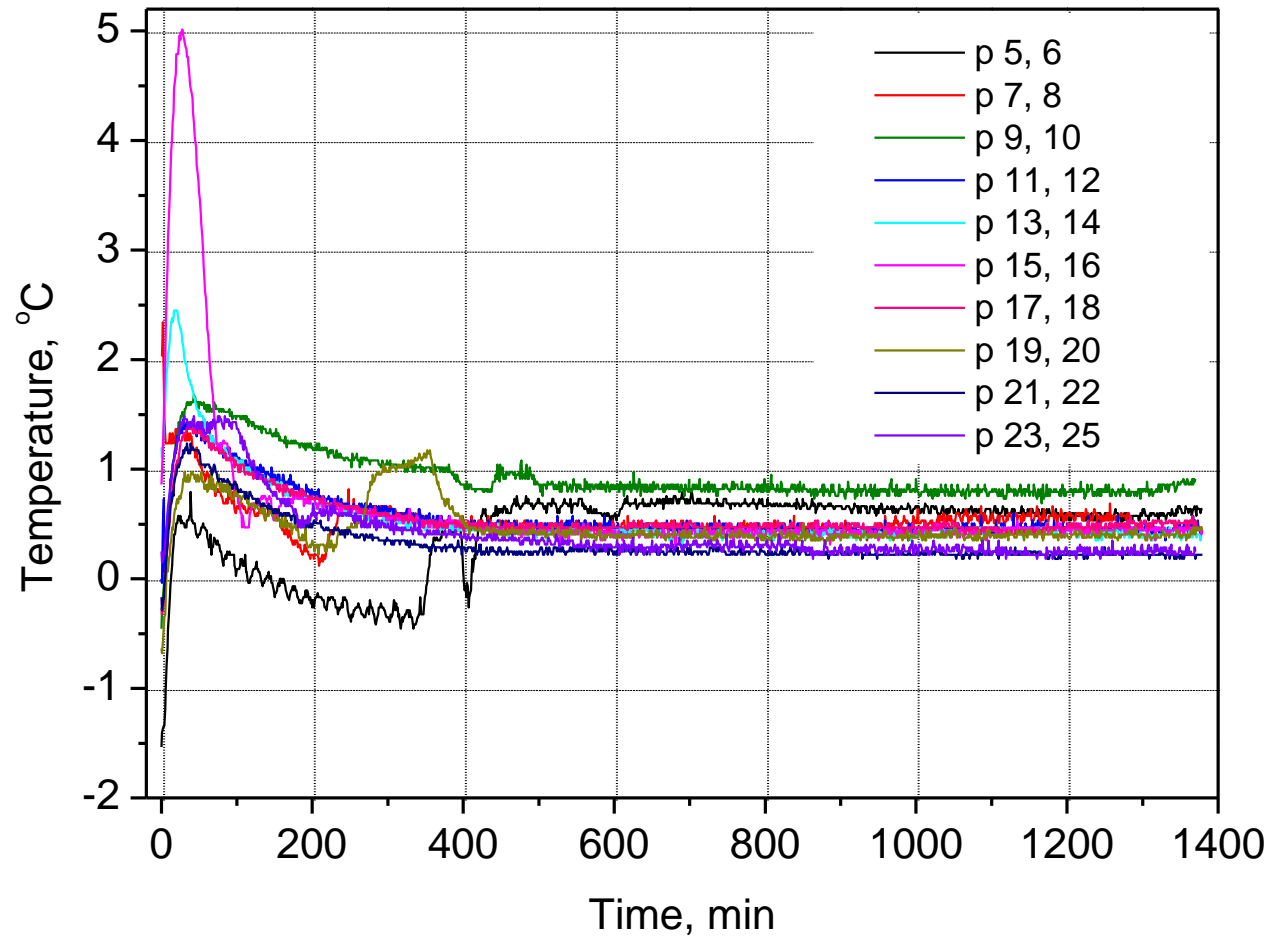


Al

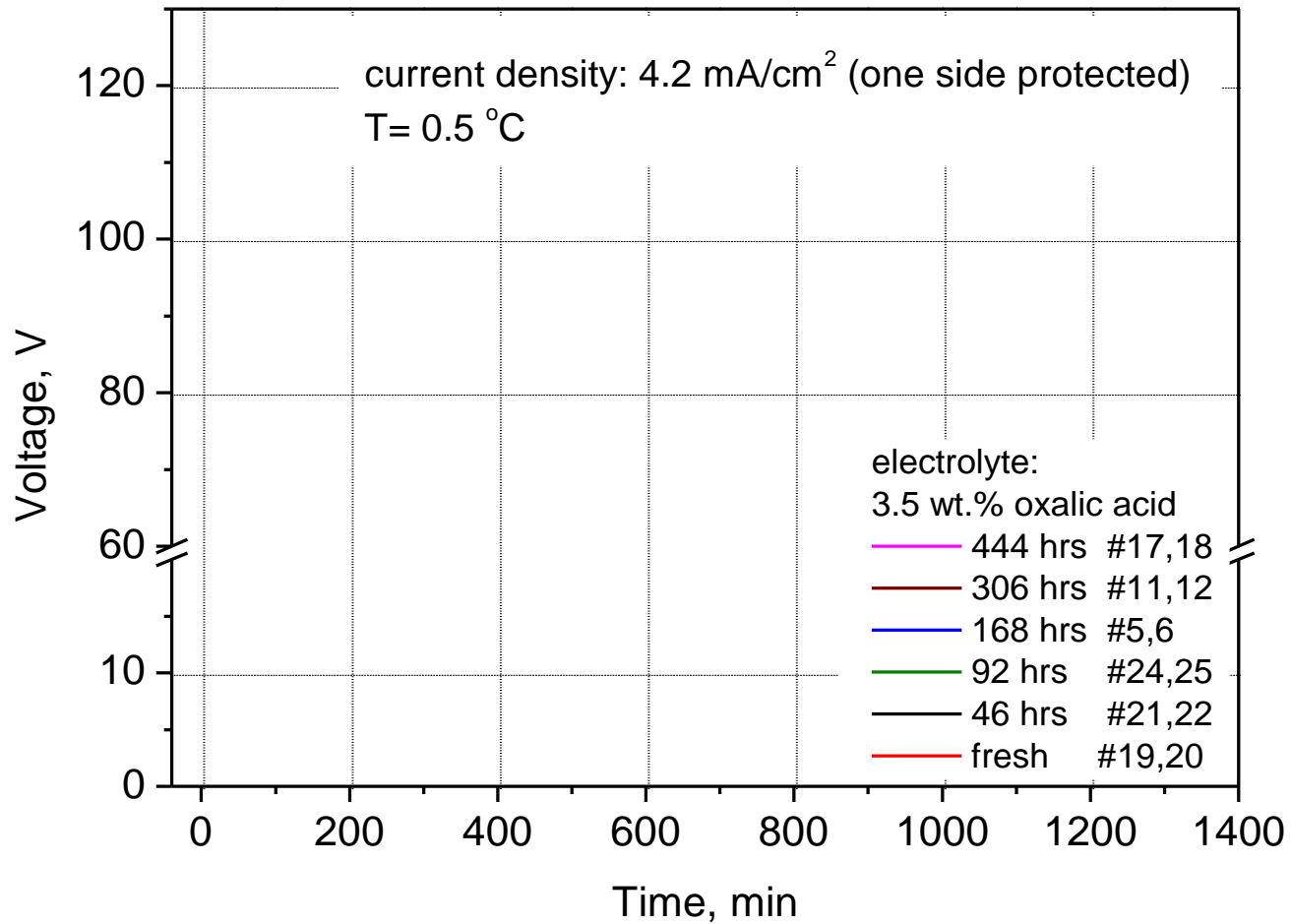
$\gamma\text{-Al}_2\text{O}_3$   
catalyst support



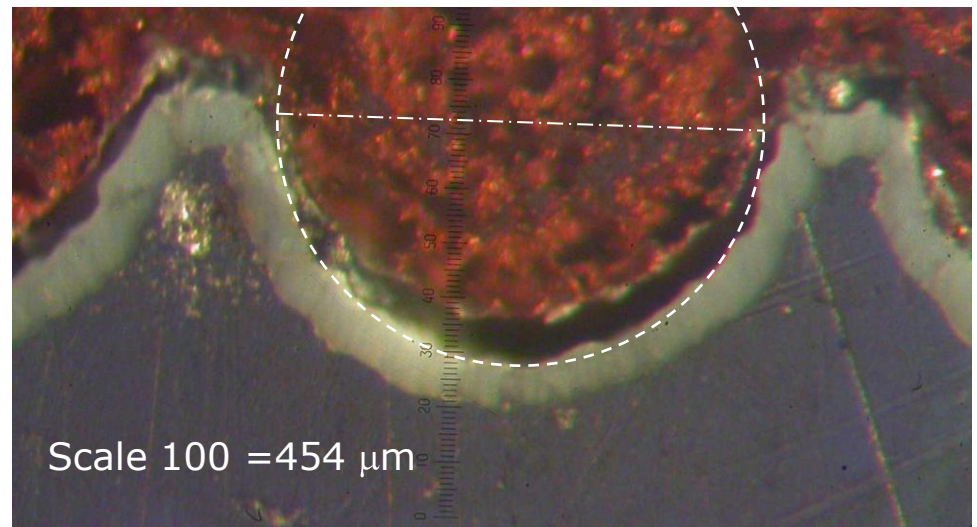
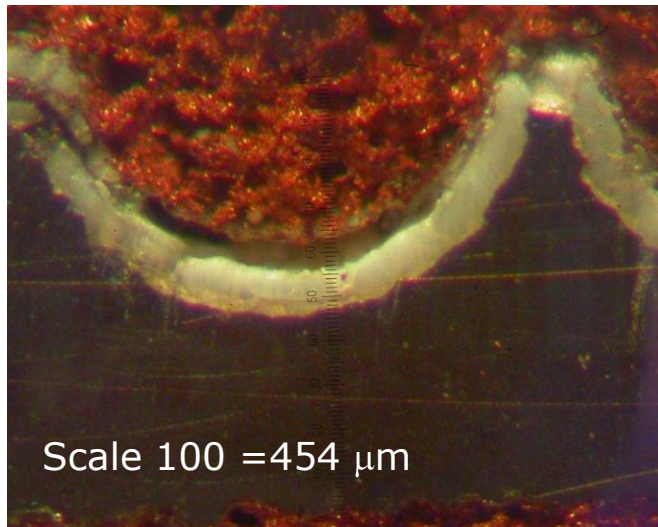
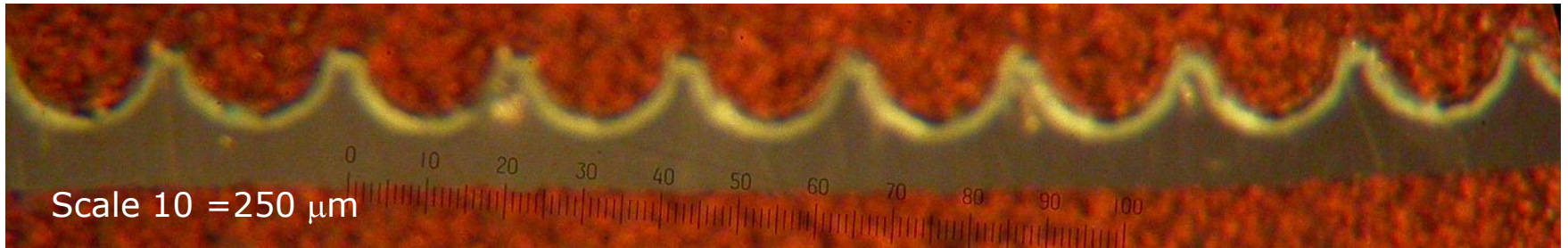
# Temperature vs. time



# Voltage vs. time



## Oxidation time 29 hrs

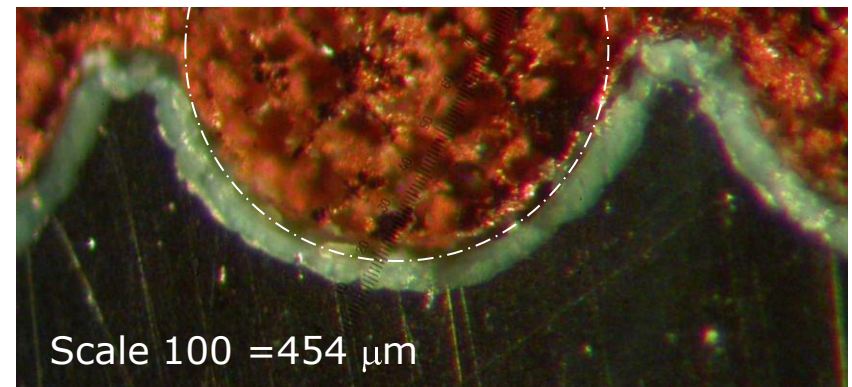
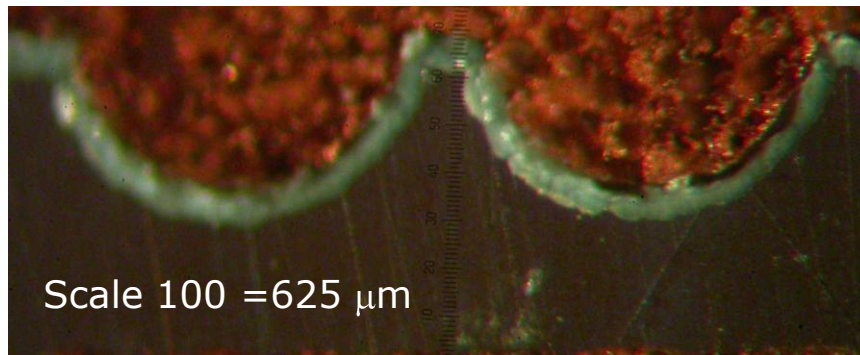
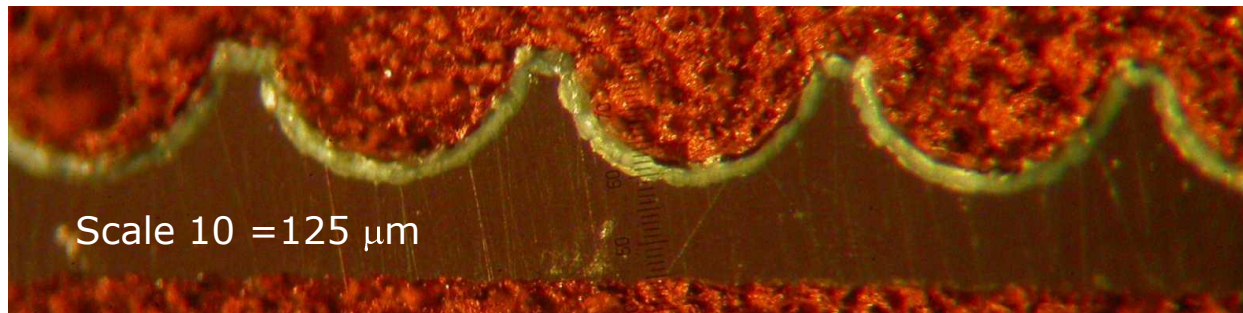
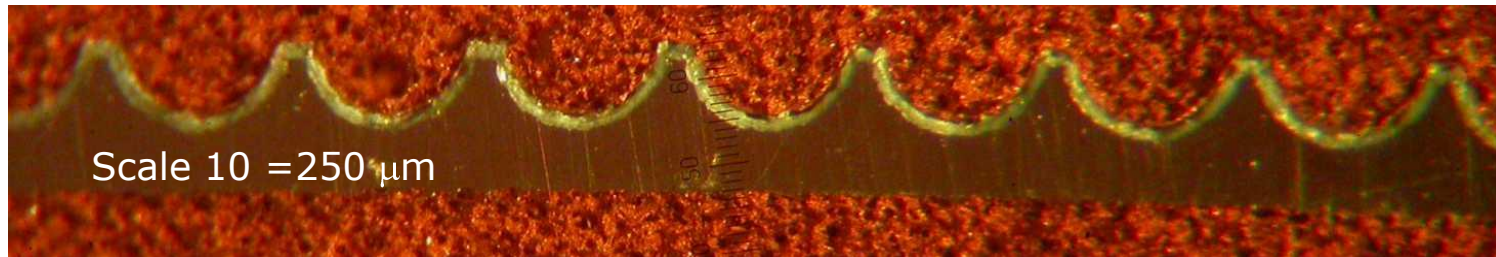


Layer thickness :  $41 \pm 1 \mu\text{m}$

R = 408  $\mu\text{m}$



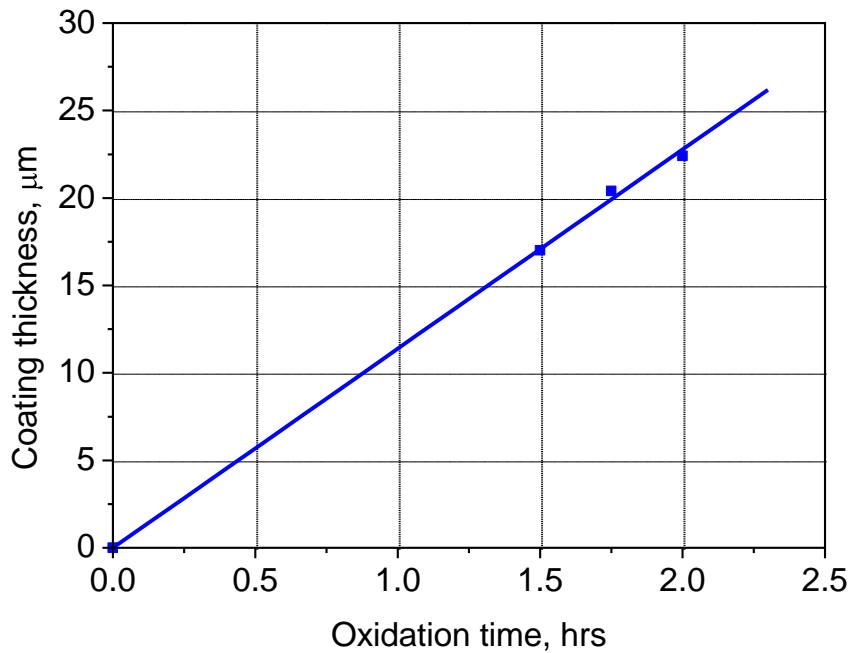
## Oxidation time 23 hrs



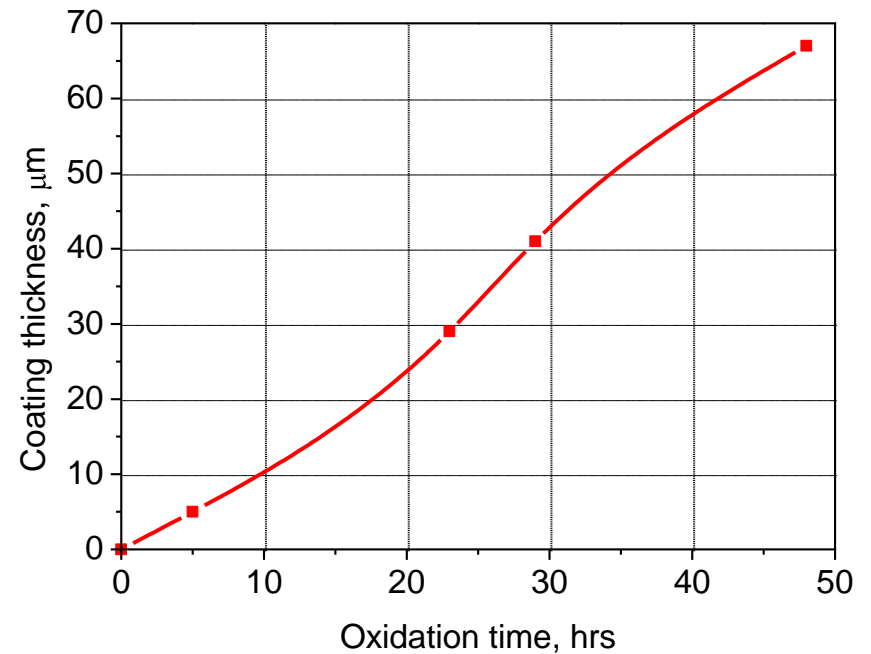
Layer thickness :  $29 \pm 1 \mu\text{m}$ ,  $R = 415 \mu\text{m}$

# Coating thickness vs. oxidation time

Flat plates

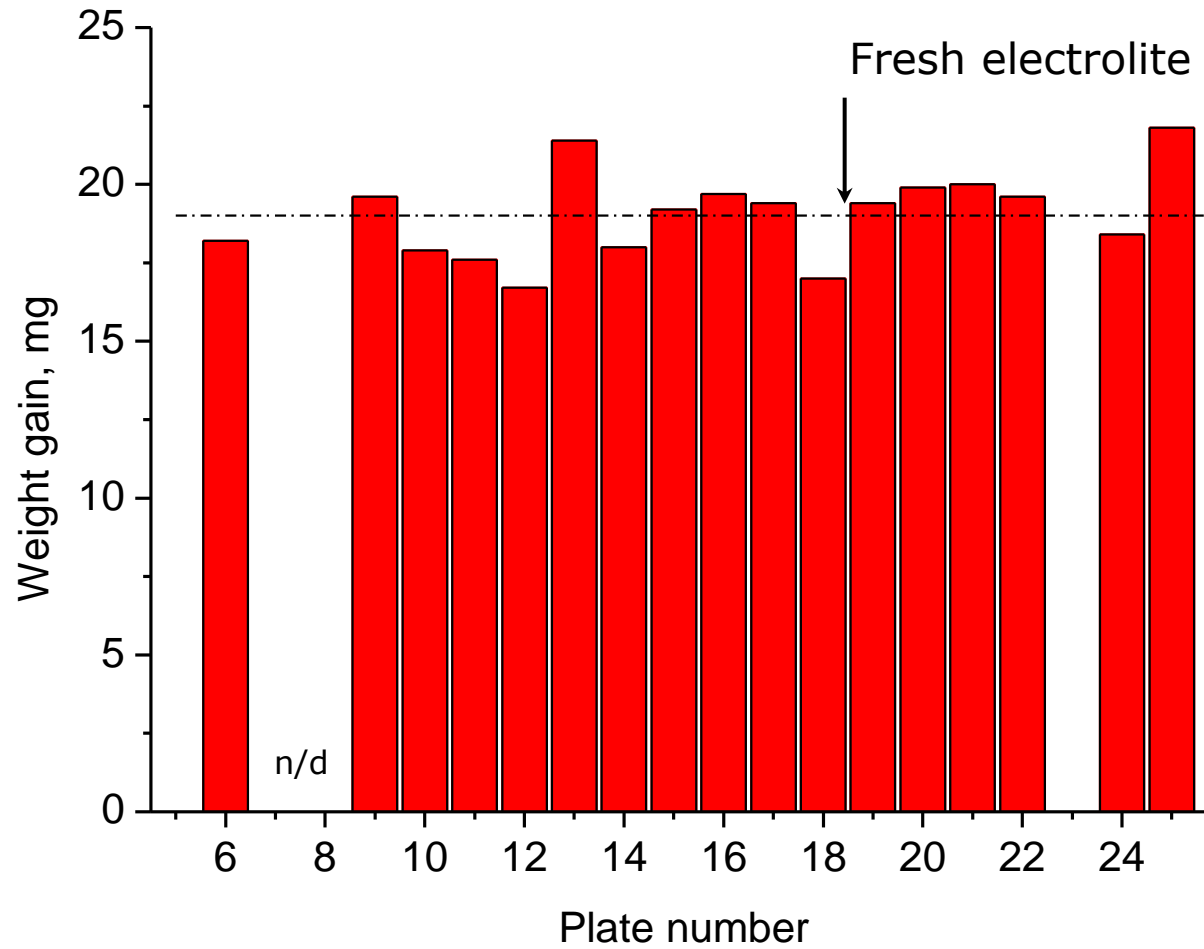


Microstructured plates



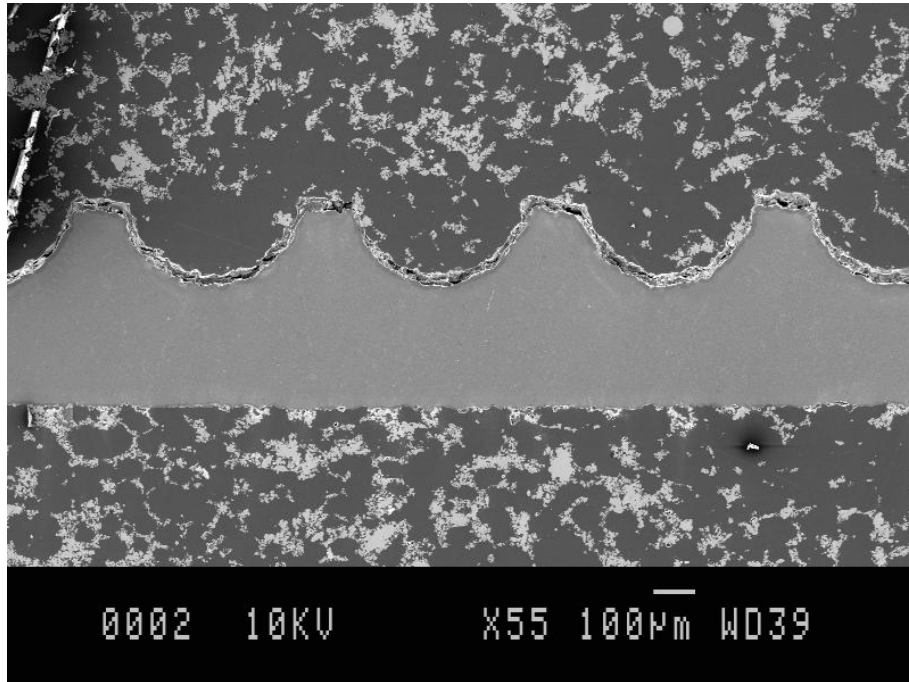


# Weight gain after routine oxidation

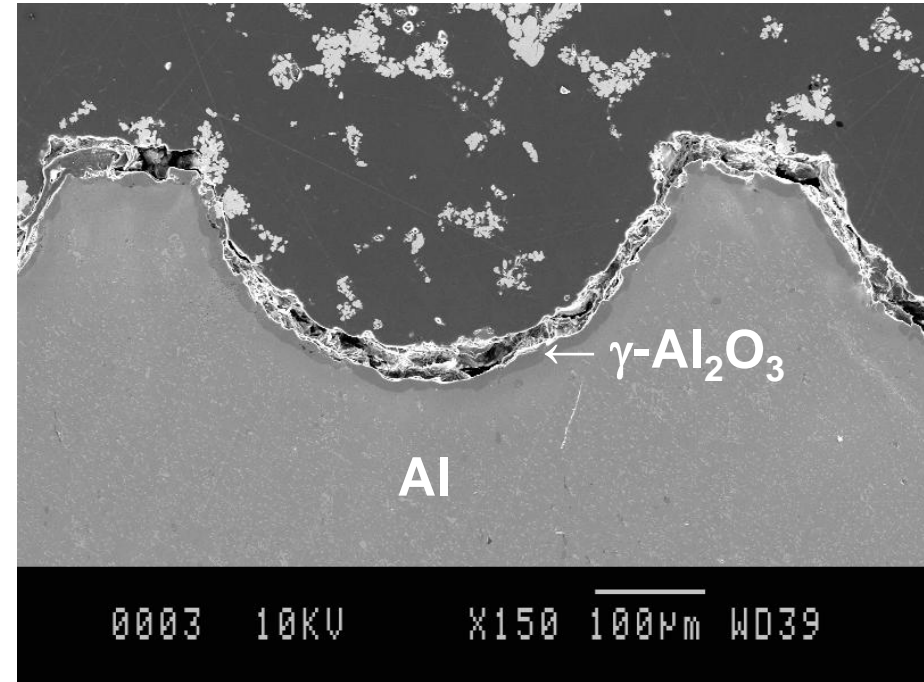


# SEM: anodic oxidation of microstructured Al plates

3 microchannels

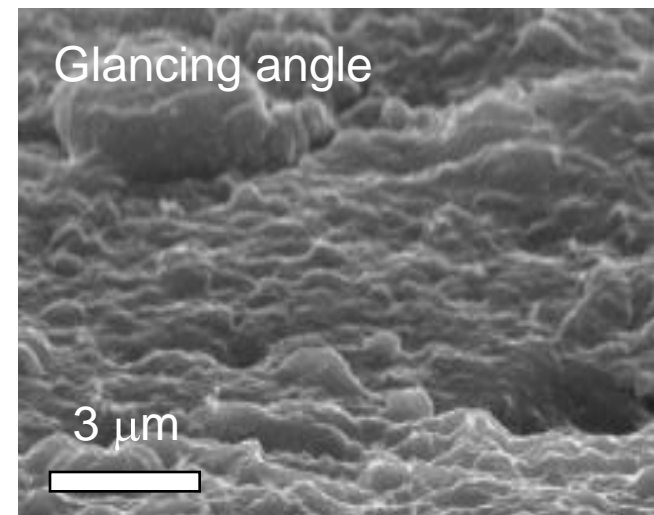
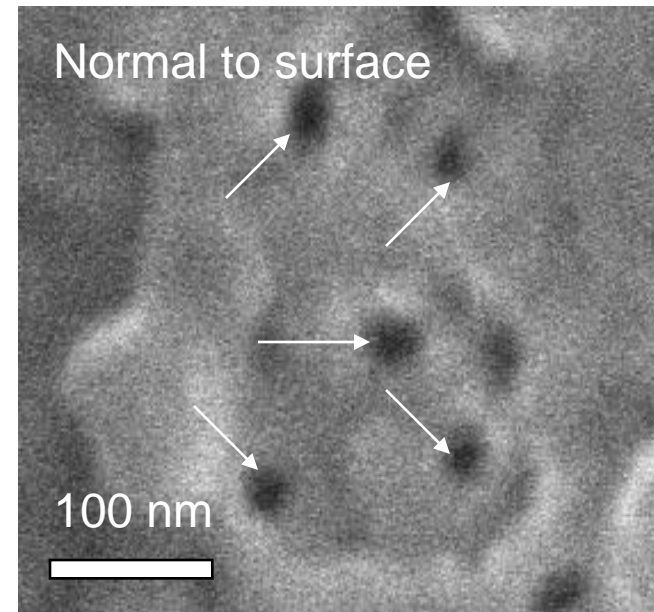
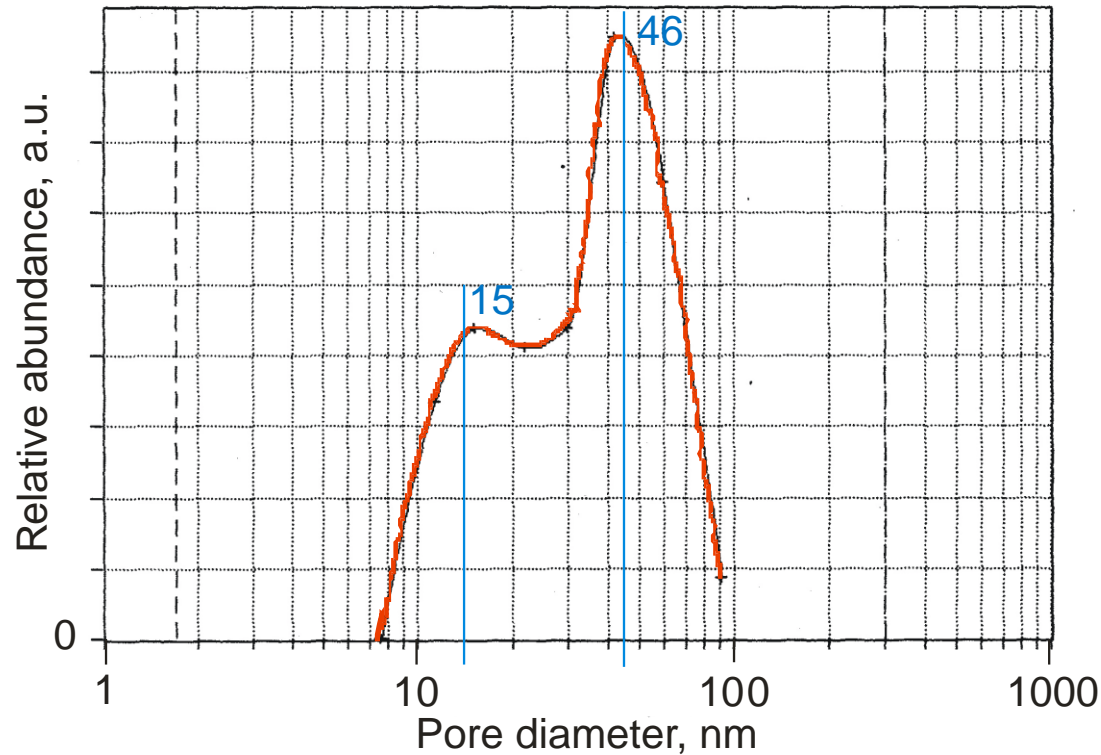


1 microchannel



15  $\mu\text{m}$  of  $\gamma\text{-Al}_2\text{O}_3$  have been formed (low thickness due to the other, non-porous  $\text{Al}_2\text{O}_3$  produced by spark erosion procedure)  $\Rightarrow$  anodic oxidation conditions are being optimized to form required 25  $\mu\text{m}$  of  $\gamma\text{-Al}_2\text{O}_3$

# Anodized flat aluminum plates: $S_{sp}$ , porosity, SEM



$S_{sp}$  ( $\gamma\text{-Al}_2\text{O}_3/\text{Al}$  plate) =  $95 \text{ m}^2/\text{cm}^3$  ( $30 \text{ m}^2/\text{g}$ ),  
pore volume  $\sim 14 \%$ , pore (cylindrical shape) distribution maxima at 15 nm and 46 nm

Result: Close to expected from literature, input data for catalyst active component deposition

## Summary

- Low current density ( $I = 4 \text{ mA/cm}^2$ ) is required for anodic oxidation of Al51 st
- Low temperature (close to the melting point of the electrolyte) is required to decrease the rate of undesirable reaction with oxalic acid
- Temperature control within  $\pm 0.5 \text{ K}$  is crucial during oxidation to get reproducible results
- Higher voltage is required in subsequent runs due to copper deposition on the cathodes and copper dissolution in the electrolyte.

# Development of spinel catalyst synthesis method using $\text{Al}_2\text{O}_3/\text{Al}$ plates

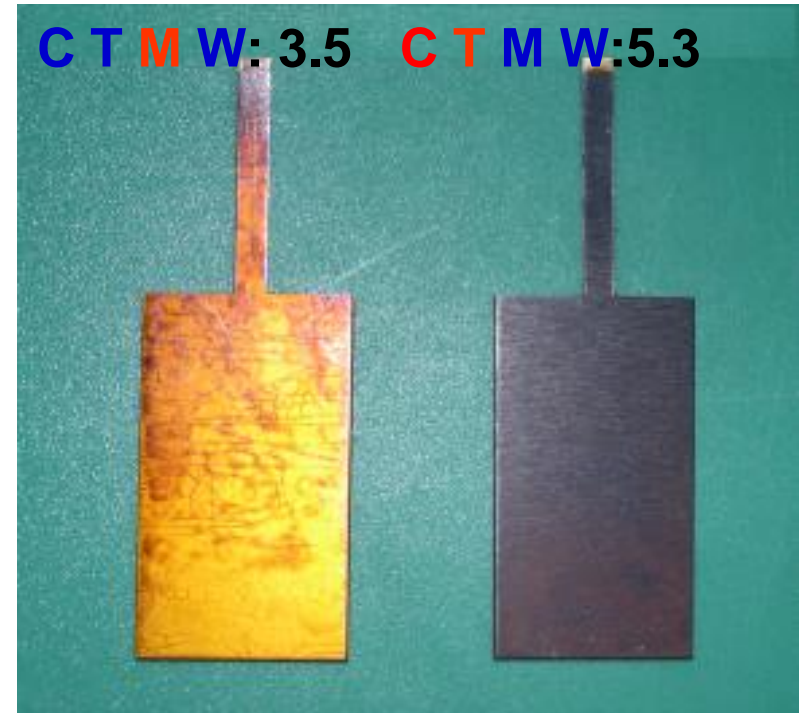
- 1. Finding initial synthesis conditions by testing different methodologies of catalyst active component deposition using conventional pelleted  $\gamma\text{-Al}_2\text{O}_3$  supports**
- 2. Synthesis using the flat plates, catalysts characterization (physical methods, catalytic activity), optimization of synthesis conditions**
- 3. Synthesis using the microstructured plates**

## Catalyst active component deposition on pelleted $\gamma\text{-Al}_2\text{O}_3$ supports

- Limiting condition: on  $\gamma\text{-Al}_2\text{O}_3/\text{Al}$  plates, catalyst calcination T not to exceed 500 °C, because m.p. of Al is ~ 600 °C (especially for microstructured Al plates)
- Method tested on pelleted (1.0-1.6 mm)  $\gamma\text{-Al}_2\text{O}_3$ : low-T formation of  $\text{CuCr}_2\text{O}_4$  spinel (impregnation with solution of copper dichromate, drying and calcination at T = 450°C for 4 h)
- XRD, BET results: at T = 450°C dominate low-T solid solutions based on spinel structure  $(\text{Cu,Cr,Al})[\text{Cr,Al}]_2\text{O}_4$  with lattice parameter  $a = 7.905\text{-}7.960$  Å, particle size  $D < 50$  Å and  $S_{\text{sp}} \sim 130$  m<sup>2</sup>/g
- Reference catalyst composition 26% $\text{CuCr}_2\text{O}_4/\gamma\text{-Al}_2\text{O}_3$

# Catalyst active component deposition on $\gamma\text{-Al}_2\text{O}_3/\text{Al}$ supports

Parameter	Level of implementation	
	Low (No*)	High (Yes*)
C of impregnation solution, g/l	<b>C</b> (250)	<b>C</b> (500)
Time of impregnation, h	<b>T</b> (0.25)	<b>T</b> (1.0)
Multiplicity of impregnations *	<b>M</b>	<b>M</b>
Washing off excess solution *	<b>W</b>	<b>W</b>



## Results:

- Washing removes most of active component ( a.c.)
- Concentrated solution – excess a.c. on surface (confirmed by XRD)
- Low concentrations deposit a.c. mostly in pores of  $\gamma\text{-Al}_2\text{O}_3$

Examples (with resulting wt.% of a.c.):

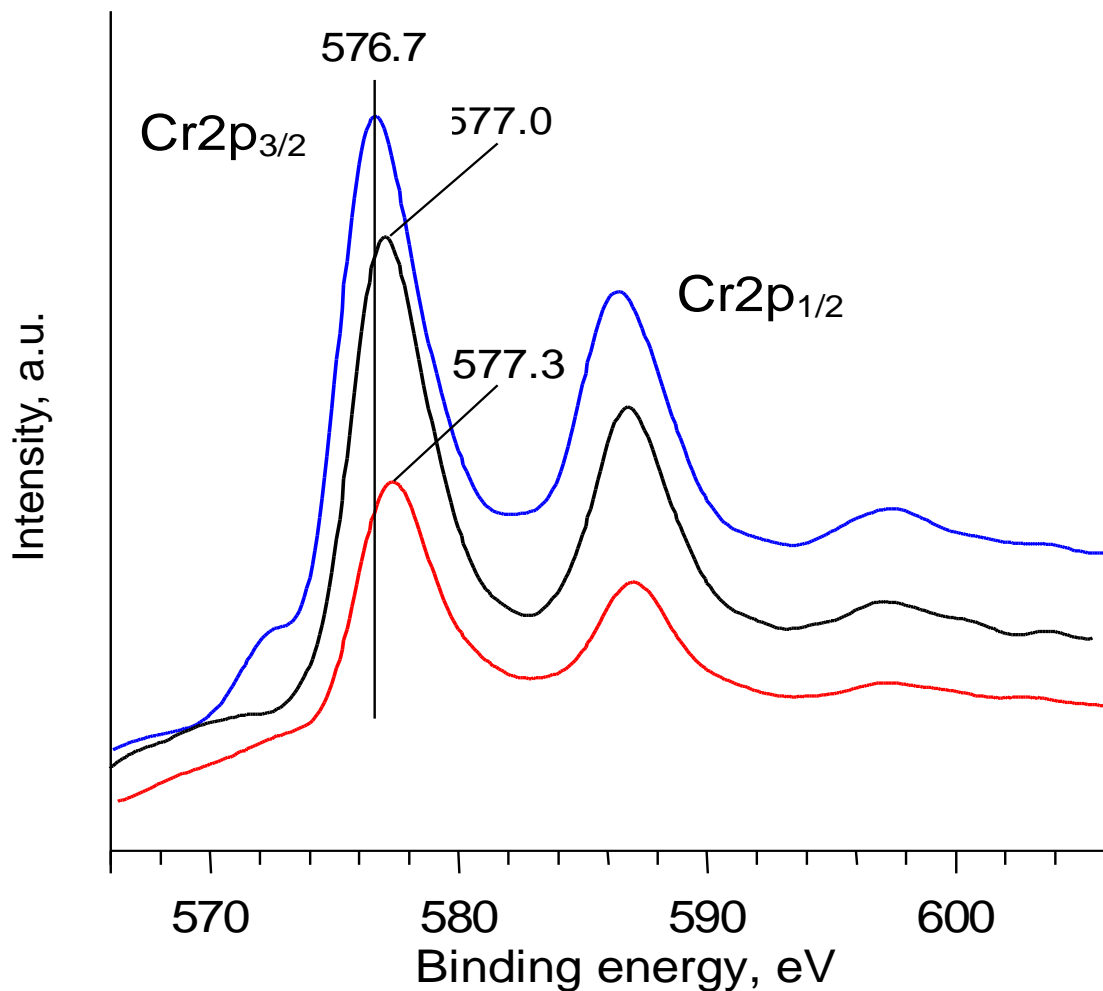
**C T M W**: 0.4

**C T M W**: 2.5

**C T M W**: 5.3



# XPS and UV-Vis: Cr cations



Normal spinels:  $XY_2O_4$   
 (X(Cu<sup>2+</sup>, T<sub>d</sub> coordination),  
 Y(Cr<sup>3+</sup>, O<sub>h</sub> coordination),  
 face-centered cubic unit cell  
 (formed by close-packed O<sup>2-</sup>))

Resulting wt.% of a.c.:

**C T M W: 5.3**

**C T M W: 3.5**

**C T M W: 0.4**

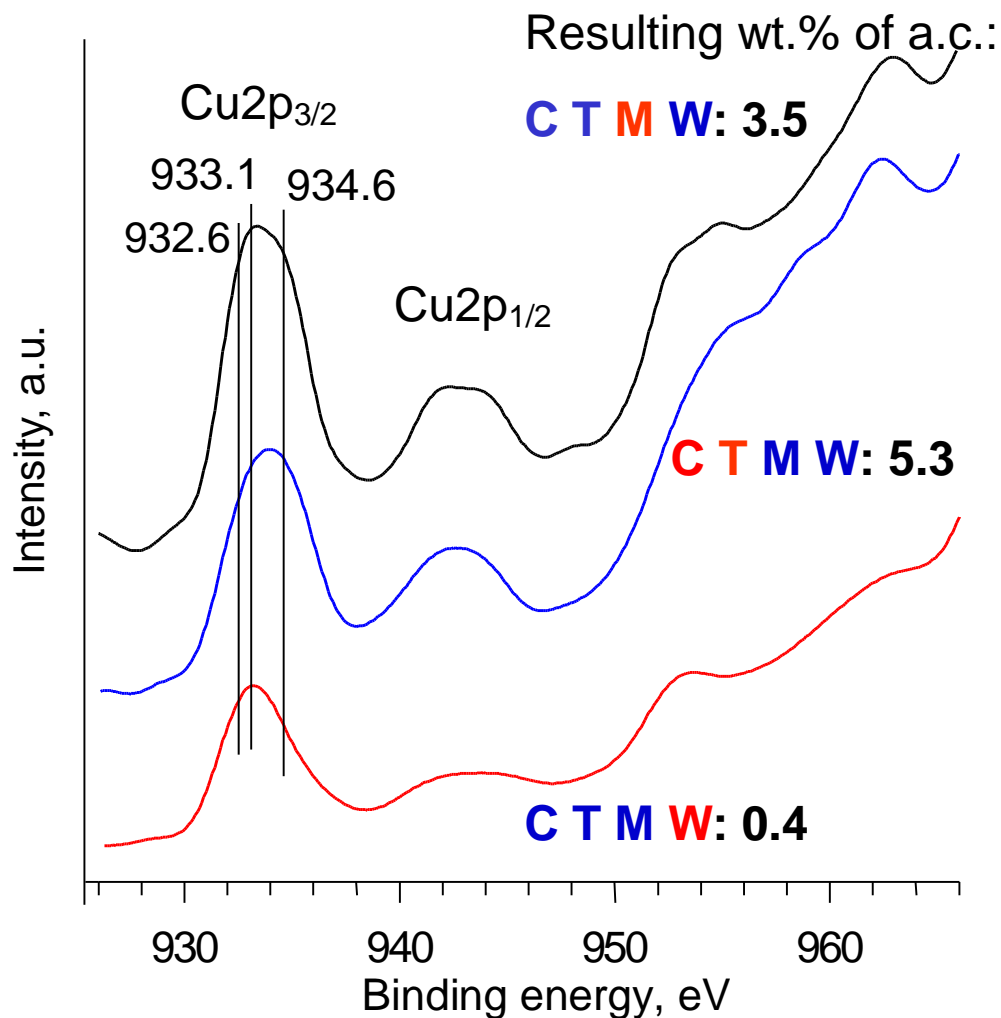
Shift to lower BE with  
 increase of active  
 component (a.c.) loading  
 => possibly, interaction  
 with  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support is  
 stronger, than within a.c.  
 particles themselves

Cr2p<sub>3/2</sub> of Cr<sup>3+</sup>: 576.5-577.5 eV (577.1 eV for CuCr<sub>2</sub>O<sub>4</sub>)

UV-Vis: O<sub>h</sub> Cr<sup>3+</sup> ~ 17000 cm<sup>-1</sup> and ~ 22000 cm<sup>-1</sup> (d-d transitions)



## XPS and UV-Vis: Cu cations



- For sample with low a.c. loading, the CuCO<sub>3</sub> signal overlaps with CuCr<sub>2</sub>O<sub>4</sub> signal, looking as 1 peak at 933.1 eV. With higher a.c. loadings, CuCO<sub>3</sub> signal becomes more pronounced

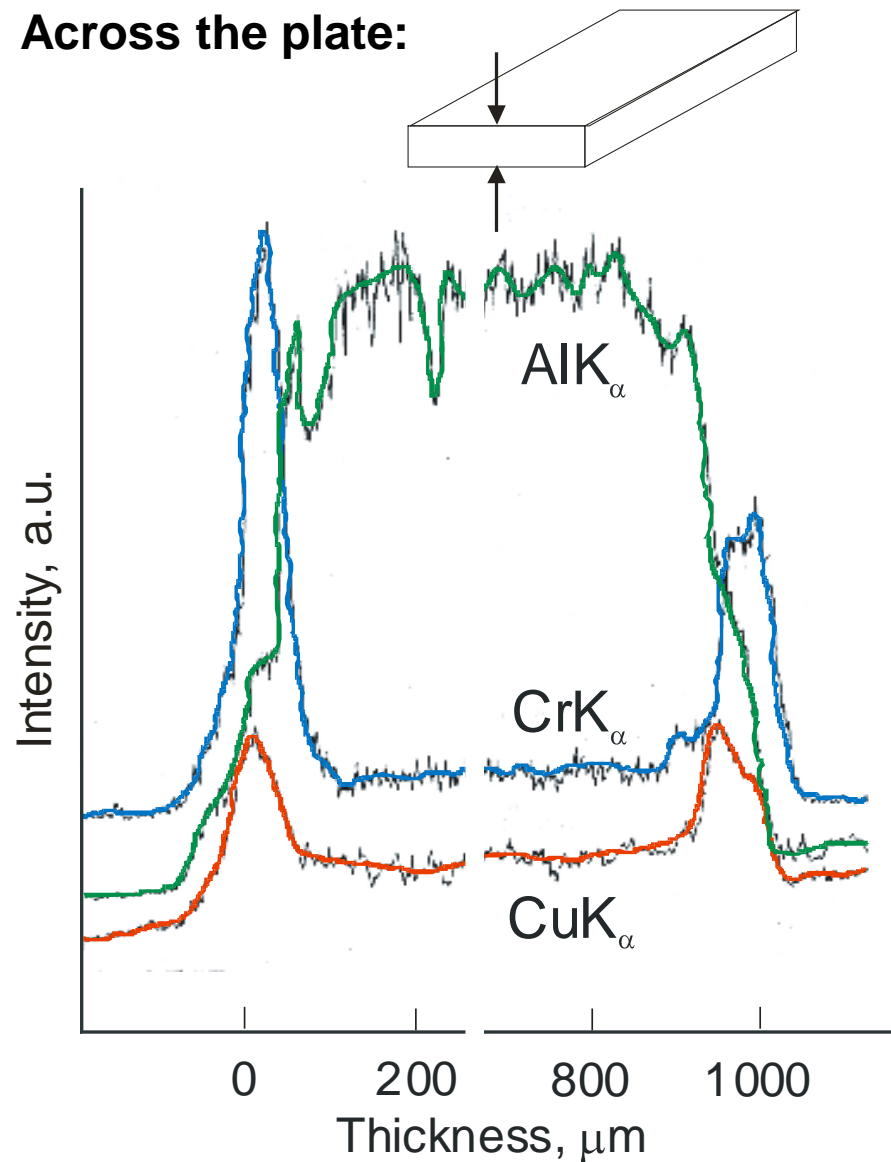
- Maximum of Cu<sup>2+</sup> content is observed for medium a.c. loading catalyst (XPS is surface-sensitive). Cu<sup>2+</sup> is considered the most active part of spinel catalyst => probably, better a.c. dispersion and Cu<sup>2+</sup> localization for this catalyst

- Shift to higher BE with increase of a.c. loading – opposite to Cr<sup>3+</sup>

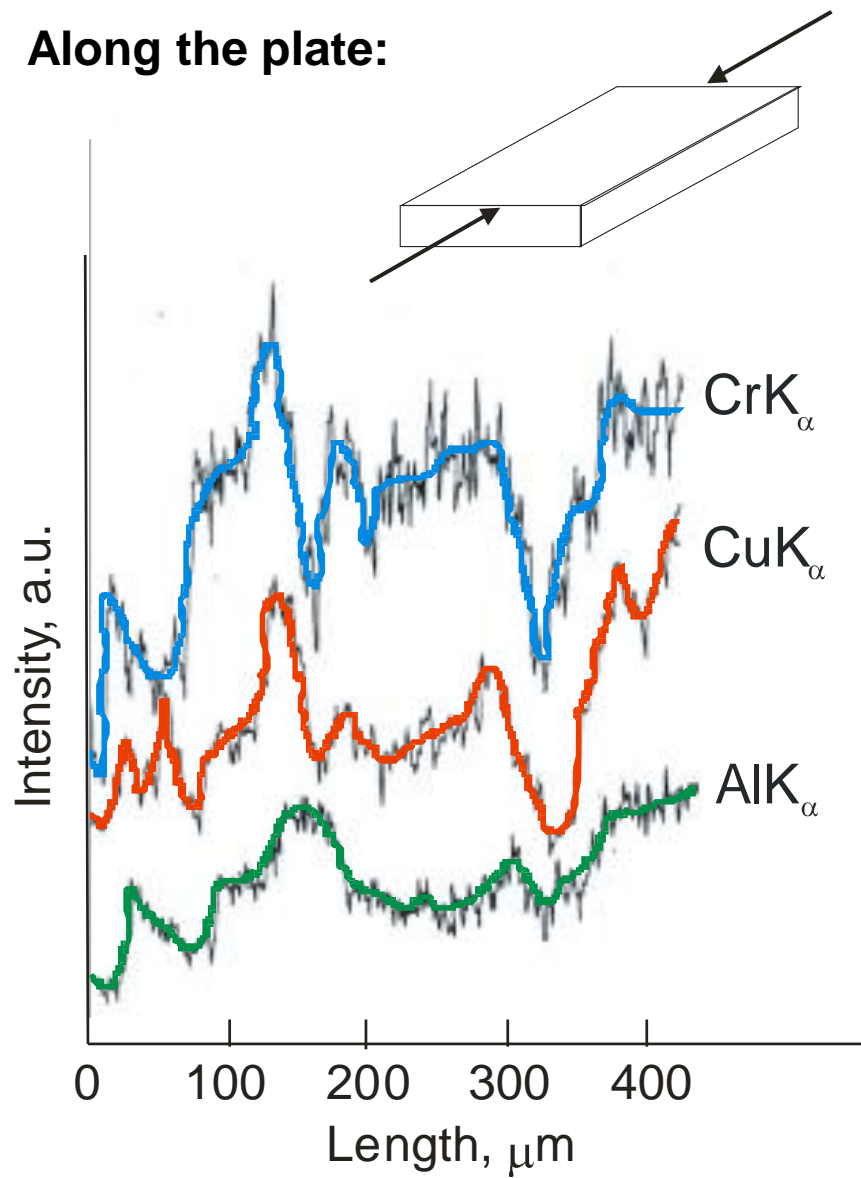
Cu $2p_{3/2}$  of Cu<sup>2+</sup>: ~ 933 eV for CuCr<sub>2</sub>O<sub>4</sub>, ~ 935 eV for CuCO<sub>3</sub>  
UV-Vis: T<sub>d</sub> Cu<sup>2+</sup> ~ 13000 cm<sup>-1</sup> (d-d transitions)

# XMA: Cu, Cr, Al distributions (sample **C T M W**: 3.5%CuCr<sub>2</sub>O<sub>4</sub>)

Across the plate:

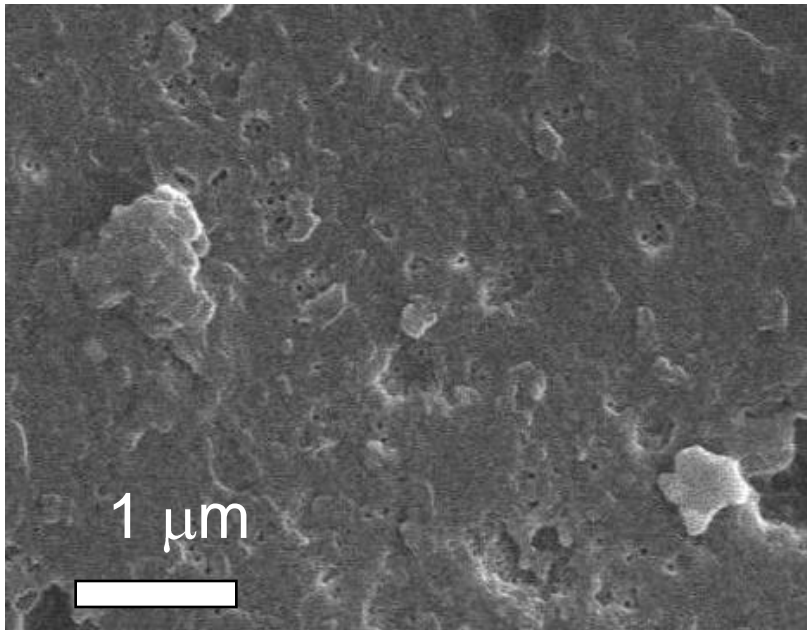


Along the plate:

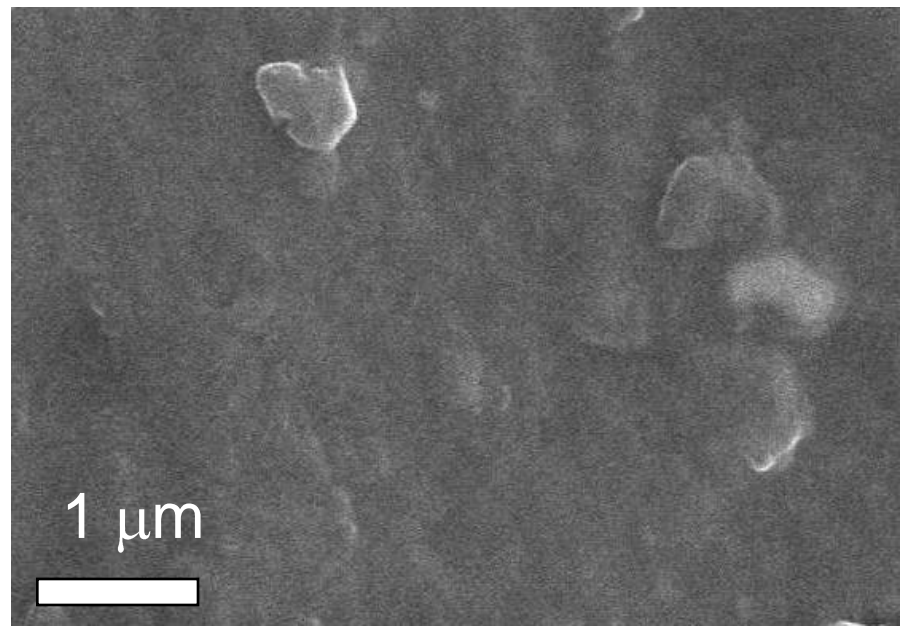


SEM:  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> surface  
before and after impregnation with CuCr<sub>2</sub>O<sub>7</sub>

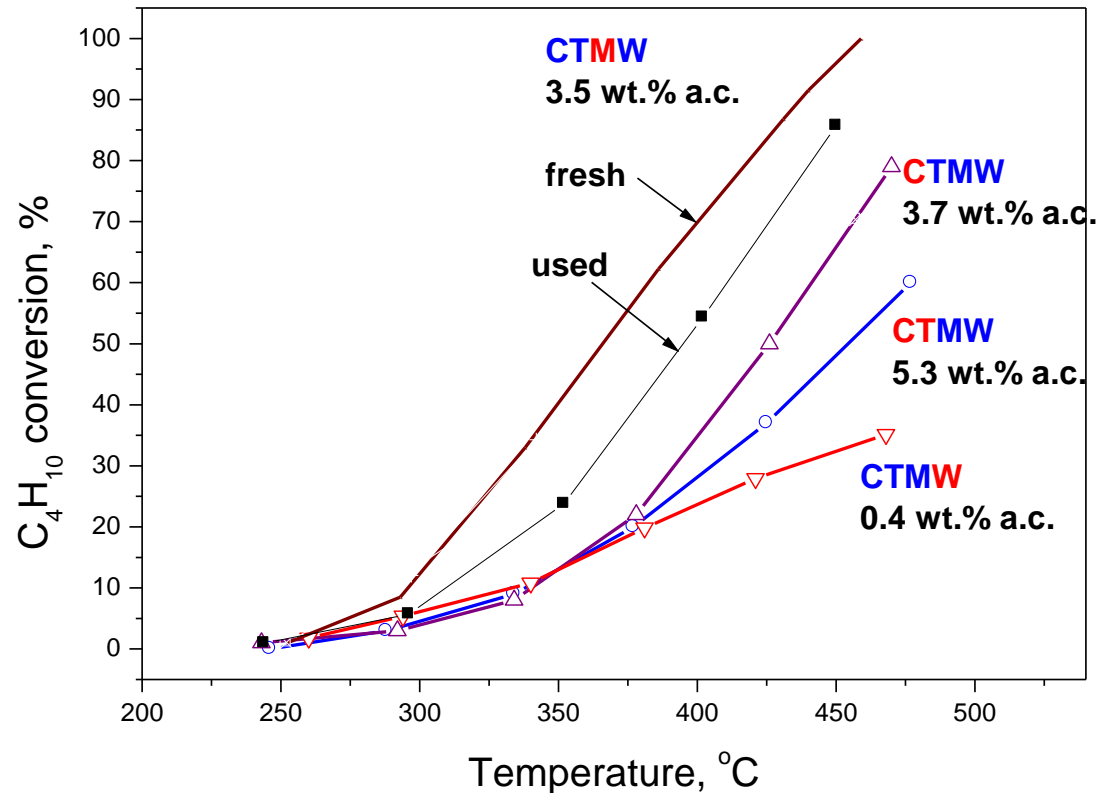
Before:  
cylindrical pores are clearly visible



After (sample **C T M W**: 5.3%CuCr<sub>2</sub>O<sub>4</sub>):  
surface is covered with CuCr<sub>2</sub>O<sub>7</sub>



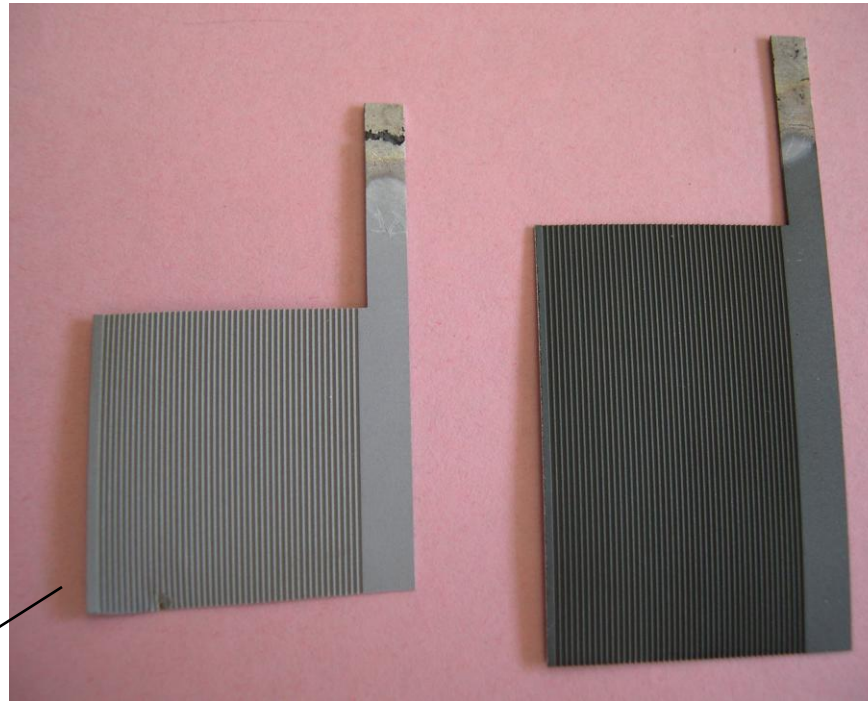
# Catalytic activity: deep oxidation of $C_4H_{10}$ on flat plate supported catalyst



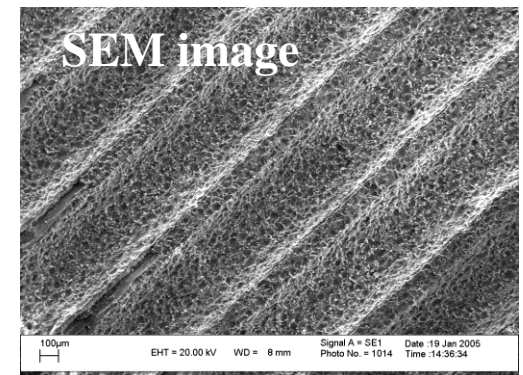
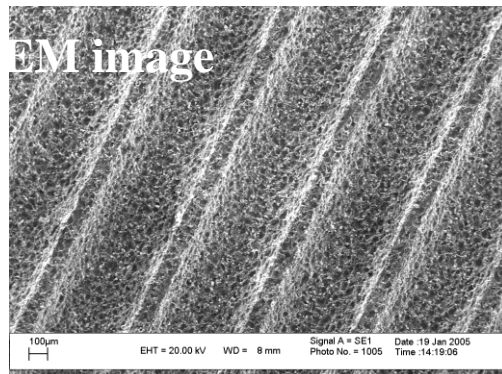
initial  $C(C_4H_{10}) = 2000$  ppm in air, GHSV =  $120000 \text{ h}^{-1}$  with respect to volume of catalytic coating

# Catalyst active component deposition on microstructured plates

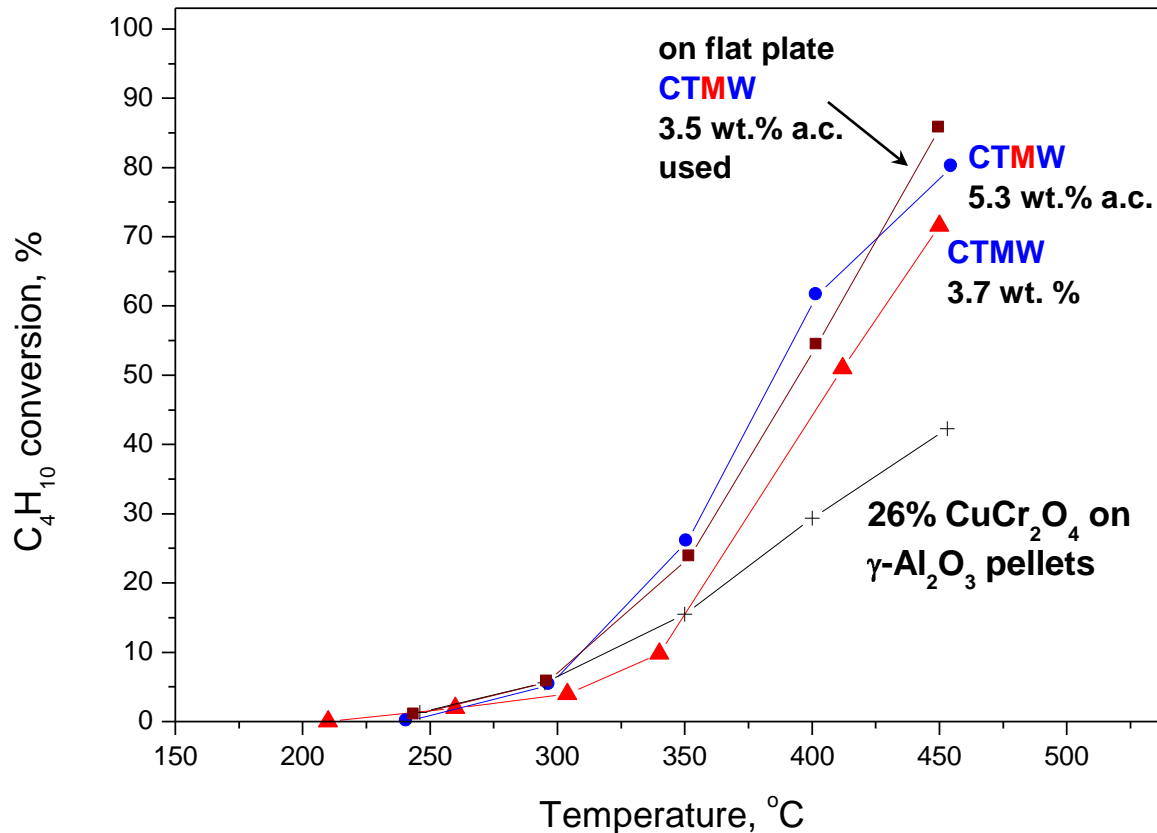
anodized  
AlMgSiCu-alloy  
plate without  
catalytic coating



CTMW  
3.7 wt. %  
 $\text{CuCr}_2\text{O}_4$

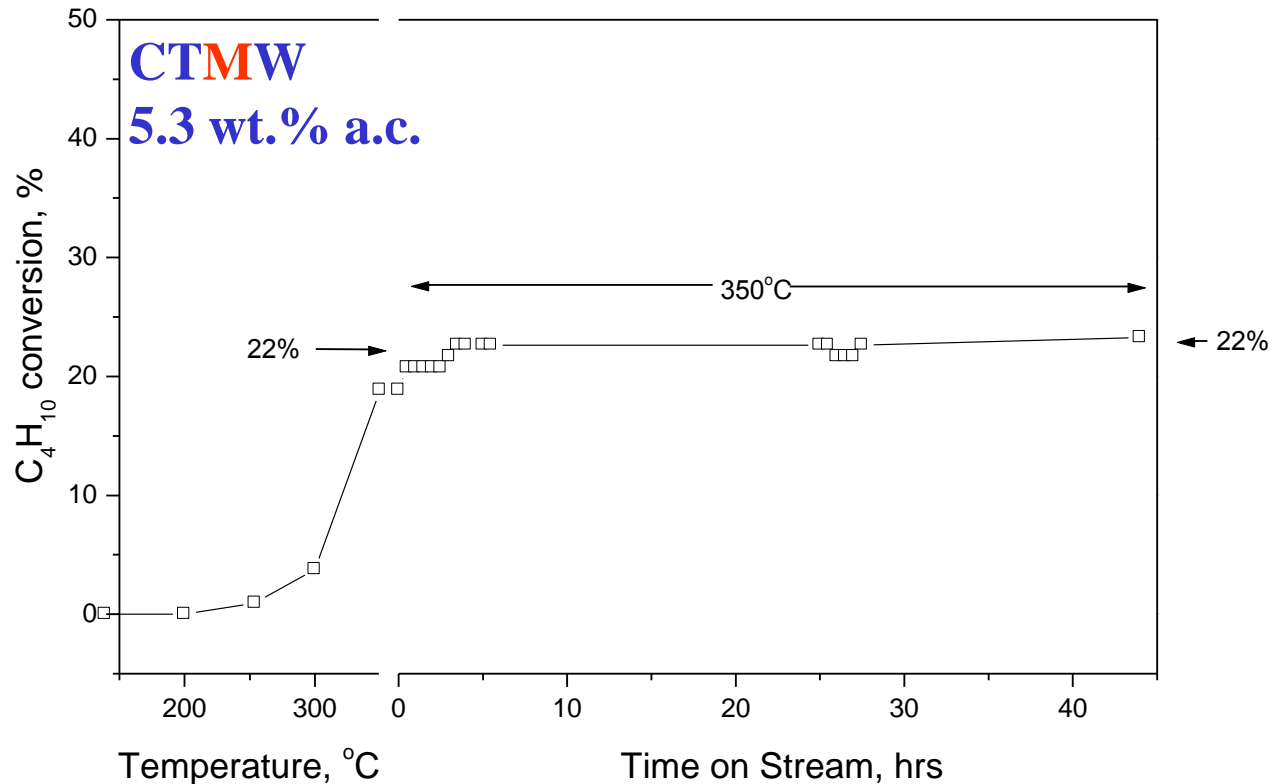


# Catalytic activity: deep oxidation of $C_4H_{10}$ on microstructured plate supported catalyst



$C(C_4H_{10}) = 2000$  ppm in air, GHSV =  $120000\text{ h}^{-1}$  with respect to volume of catalytic coating

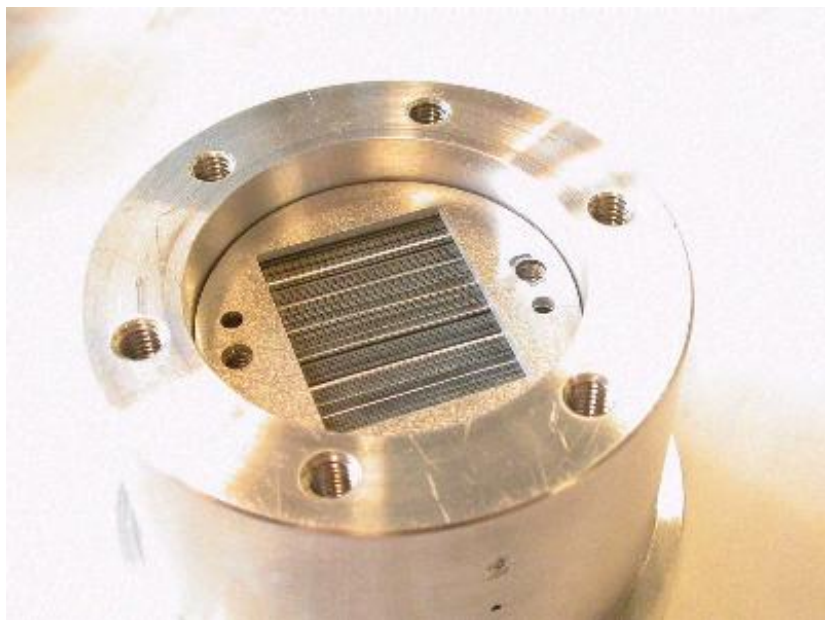
# Catalytic activity: deep oxidation of $C_4H_{10}$ on microstructured plate supported catalyst



initial  $C(C_4H_{10}) = 2000$  ppm, GHSV =  $120000 \text{ h}^{-1}$  vs.  $\gamma\text{-Al}_2\text{O}_3$  with respect to volume of catalytic coating



# Catalytic microreactor for total oxidation reactions





## Conclusions

- 1. The alumina-supported Cu, Cr oxide catalysts for reactions of total oxidation in a microreactor were synthesized using flat and microstructured anodized Al plates and characterized**
- 2. The formation of  $\text{CuCr}_2\text{O}_4$  active component on  $\gamma\text{-Al}_2\text{O}_3/\text{Al}$  plates produced by anodic oxidation was confirmed by XPS, UV-Vis, XRD, XMA and SEM**
- 3. The best catalyst synthesis method is via double impregnation for 15 min with a diluted aqueous solution of copper dichromate**
- 4. The  $\text{C}_4\text{H}_{10}$  oxidation activities of coatings even at much less content of active component are superior to that of the reference pelleted catalyst**

## Acknowledgements



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**for the financial support of this Project**